

Battery-Free Antenna Sensors for Strain and Crack Monitoring of Bridge Structures

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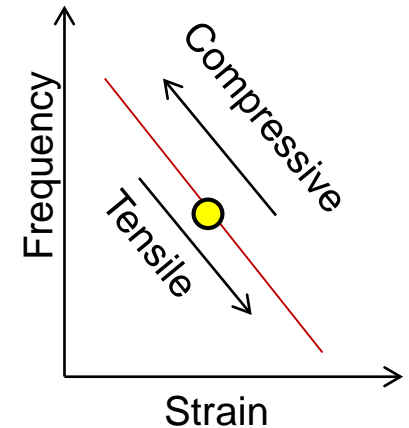
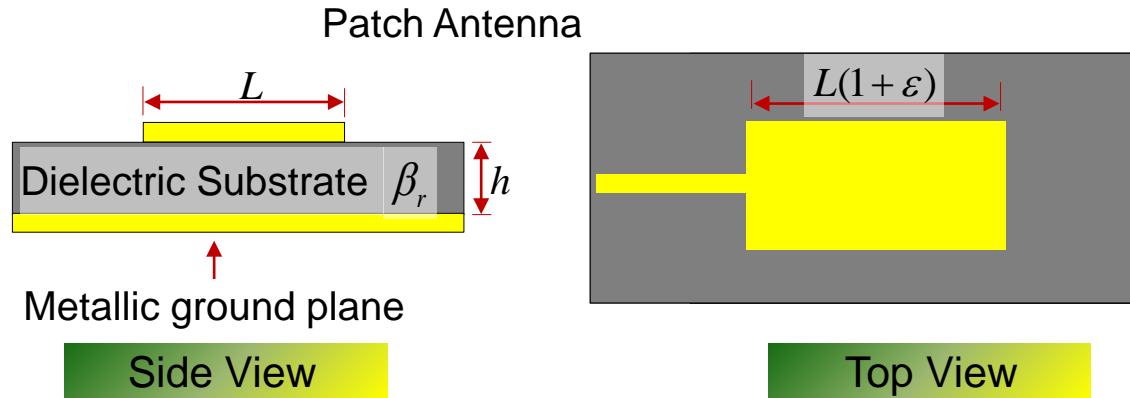
INSPIRE UTC, Rolla, MO

August 14, 2018

Outline

- ❑ Research Background & Motivation
- ❑ Thermal Stability Tests
 - Temperature Chamber Test
 - Day-long Outdoor Test
- ❑ Material Property Tests
 - Constitutive Relationship of Substrate
 - Constitutive Relationship of Glue
 - Dielectric Constant of Substrate
- ❑ Multi-Physics Simulation
- ❑ Validation Tests
 - Strain Sensing Test
 - Crack Sensing Test
- ❑ Conclusion

Strain Sensing Mechanism



Electromagnetic resonance frequency of a patch antenna (at zero strain):

$$f_{R0} \approx \frac{c}{2L\sqrt{\beta_r}}$$

c -- speed of light

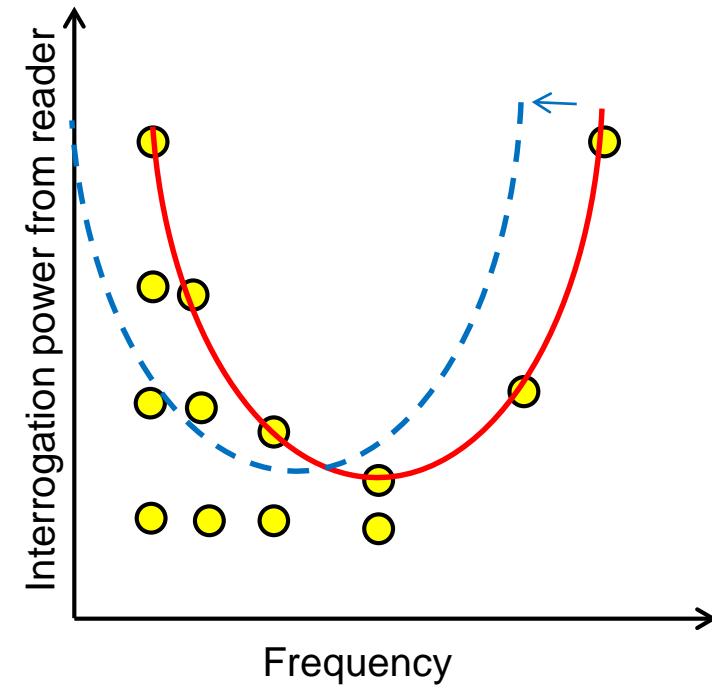
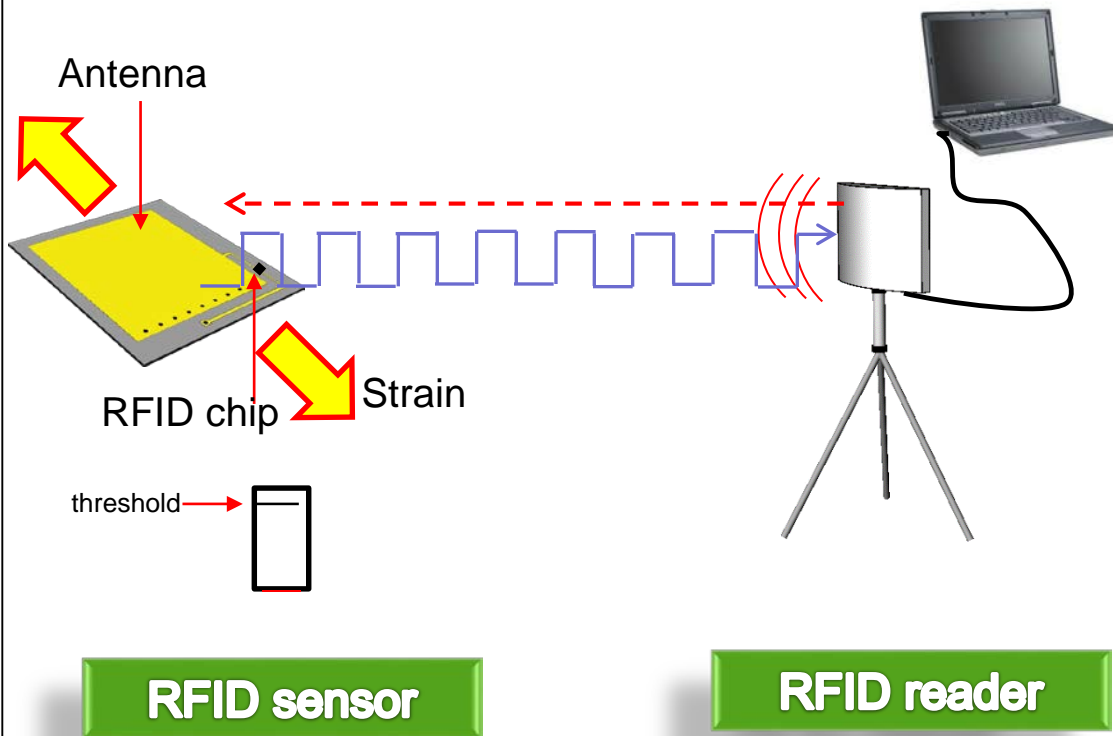
L -- length of microstrip patch antenna (half wavelength)

β_r -- effective dielectric constant of the antenna substrate

Under **strain** ϵ , resonance frequency shifts to $f_R \approx \frac{c}{2(1 + \epsilon)L\sqrt{\beta_r}} = \frac{f_{R0}}{1 + \epsilon} \approx f_{R0}(1 - \epsilon)$

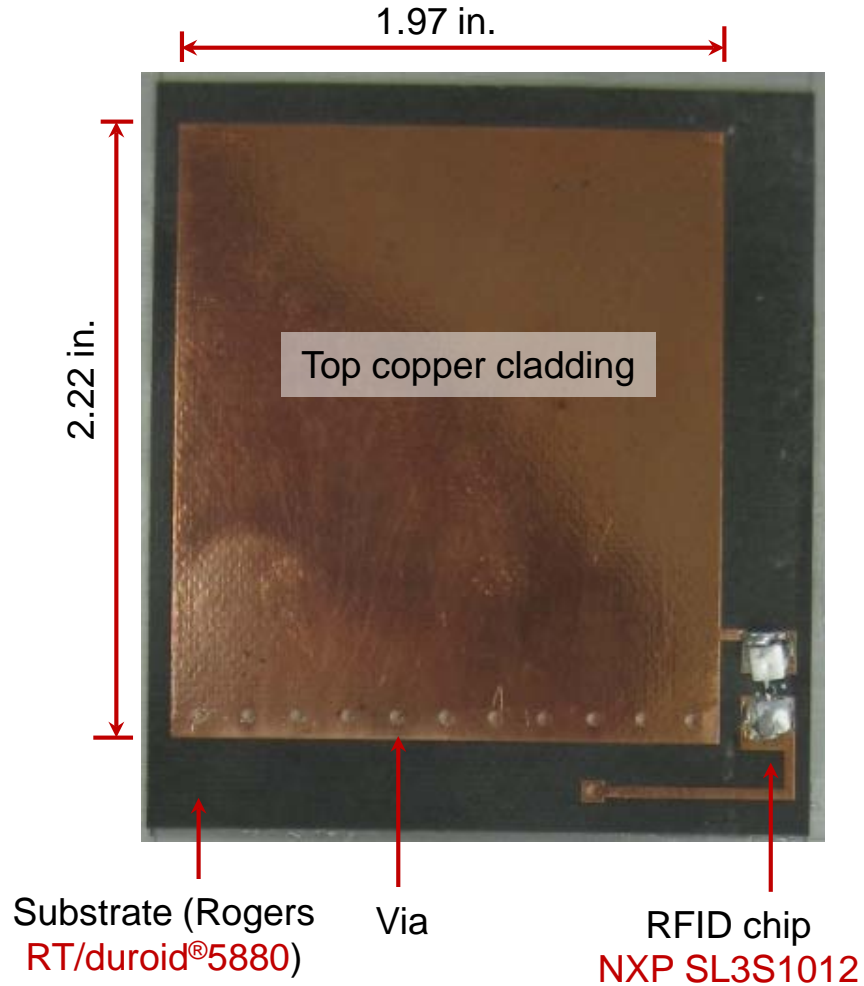
Strain sensitivity is $S = \frac{f_R - f_{R0}}{\epsilon}$ (Hz/ $\mu\epsilon$)

RFID Reader-Sensor System

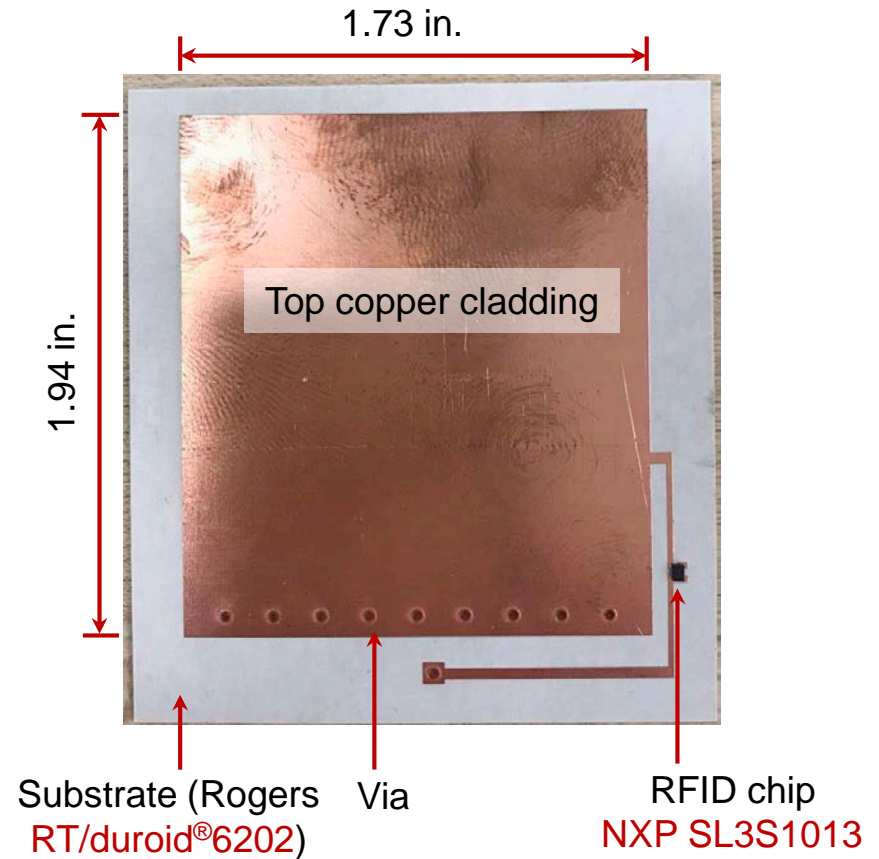


Antenna Sensor Design

Previous Design



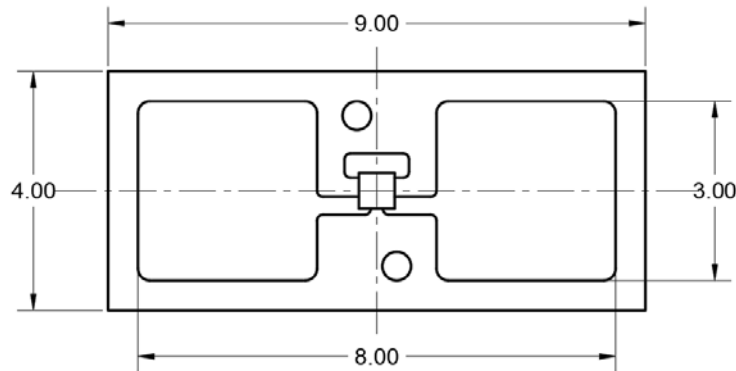
New Design



Difference from Previous Design

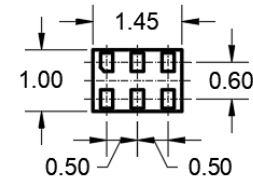
- Chip

Old chip: SL3S1002 (Unit: mm)



Impedance: $13.3-j122 \Omega$

New chip: SL3S1013 (Unit: mm)

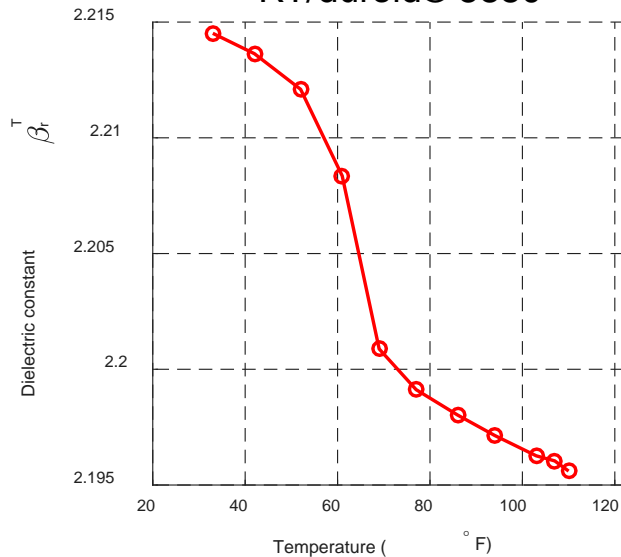


Impedance: $21.2-j199.7 \Omega$

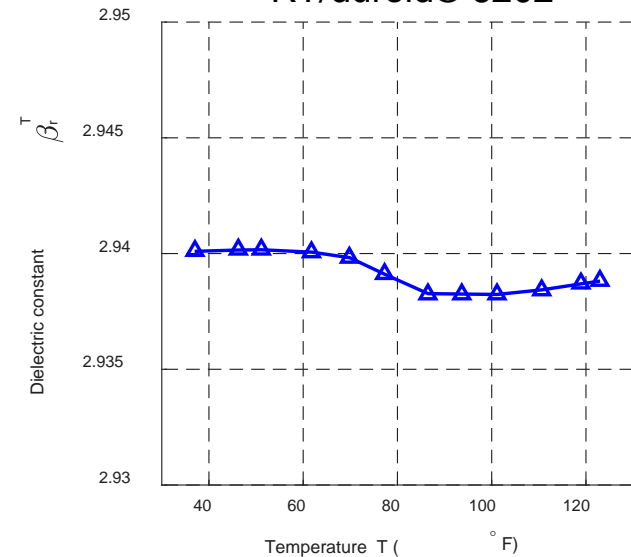
- Substrate dielectric constant β_r

$$f_{R0} \approx \frac{c}{2L\sqrt{\beta_r}}$$

RT/duroid® 5880



RT/duroid® 6202



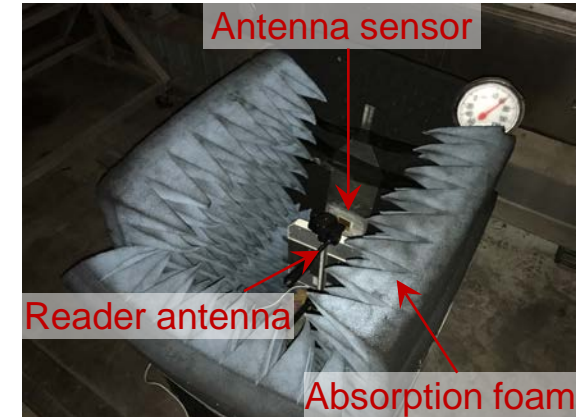
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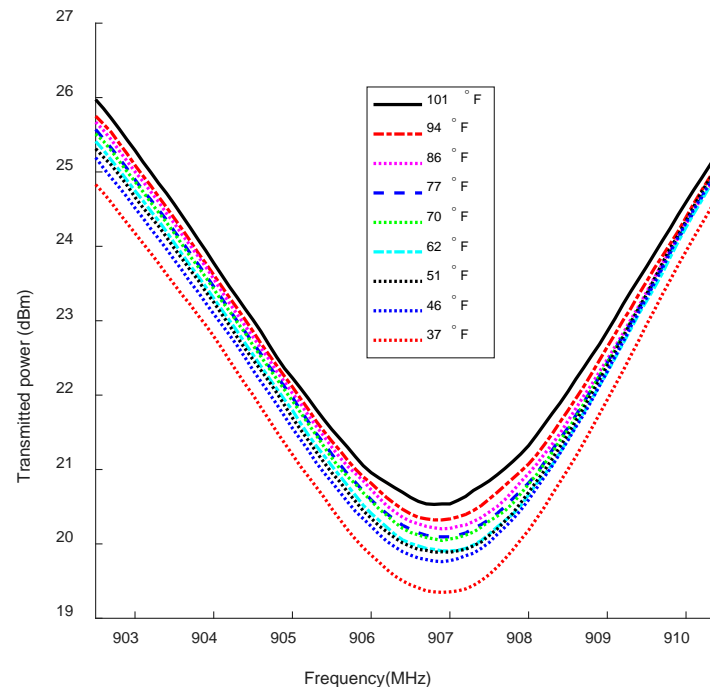
Temperature Chamber Test

- Thermal influence on the new substrate material RT/duroid® 6202 is investigated through a temperature chamber experiment.
- At each temperature step, sweep frequency band 902.5 ~ 910.5 MHz.
- From transmitted power curve, resonance frequency is extracted.
- RT/duroid® 6202 is thermally stable on dielectric constant.

Experiment setup

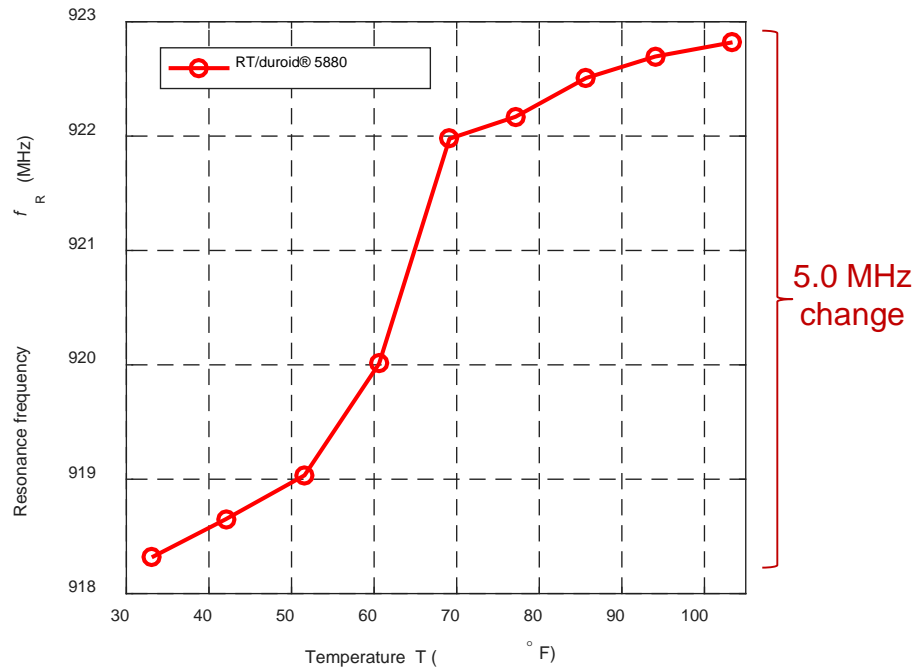


Transmitted power



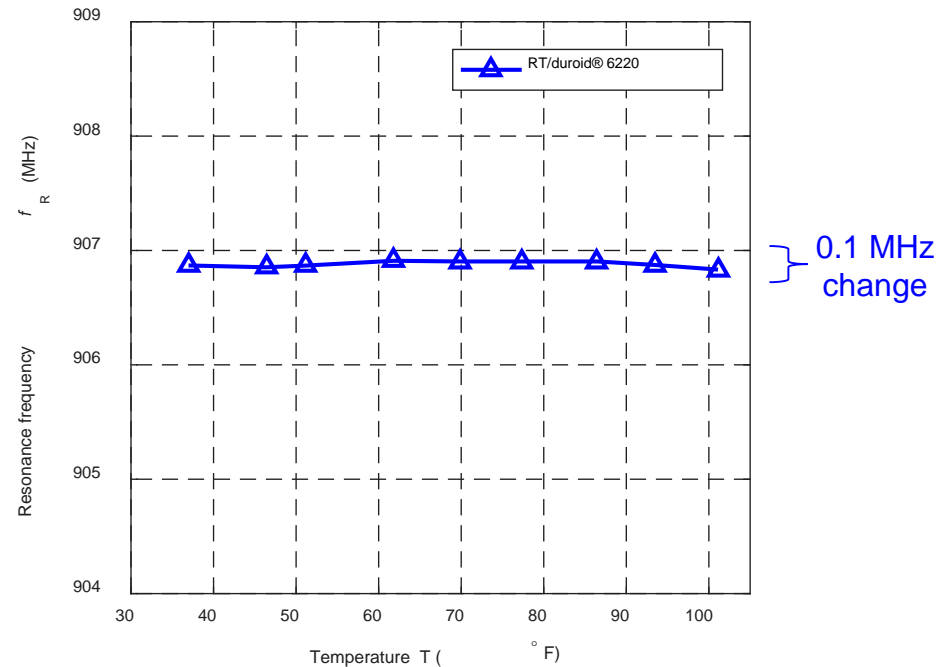
Comparison with RT/duroid® 5880

RT/duroid® 5880



Dielectric constant changes significantly due to temperature fluctuation.

RT/duroid® 6202



Dielectric constant is more stable to temperature fluctuation.

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☐ Research Background & Motivation

☐ Thermal Stability Tests

- Temperature Chamber Test
- Day-long Outdoor Test

☐ Material Property Tests

- Constitutive Relationship of Substrate
- Constitutive Relationship of Glue
- Dielectric Constant of Substrate

☐ Multi-Physics Simulation

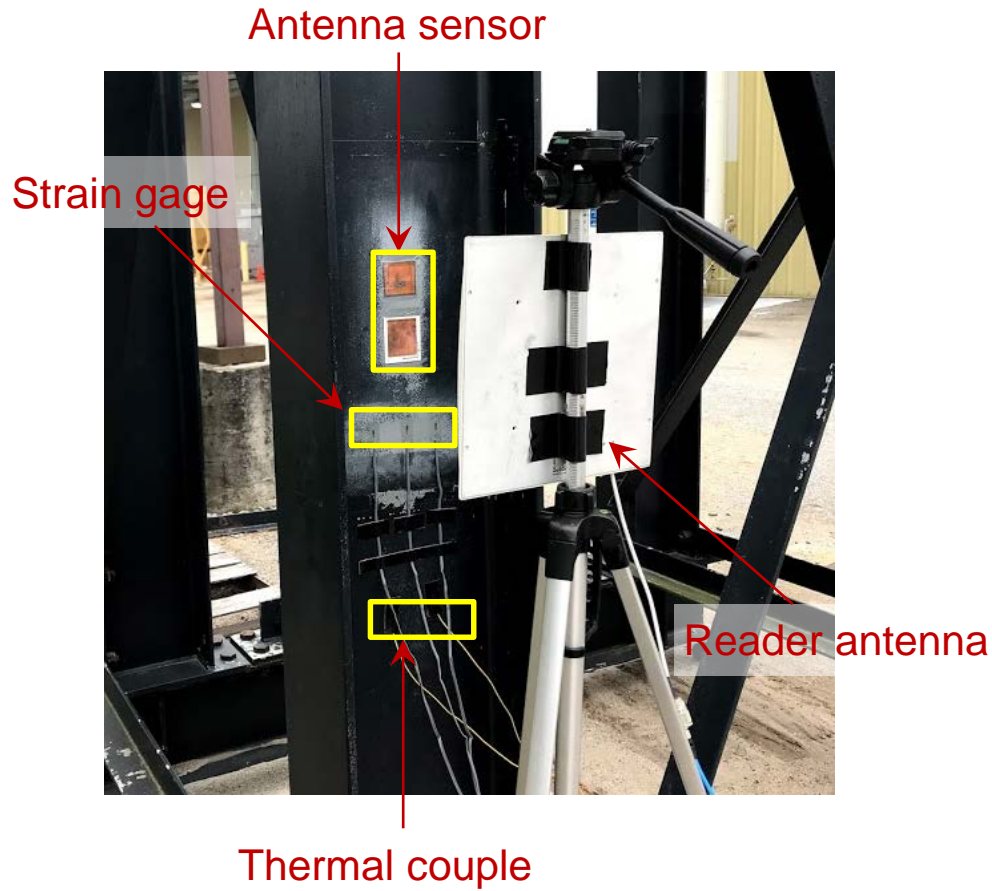
☐ Validation Tests

- Strain Sensing Test
- Crack Sensing Test

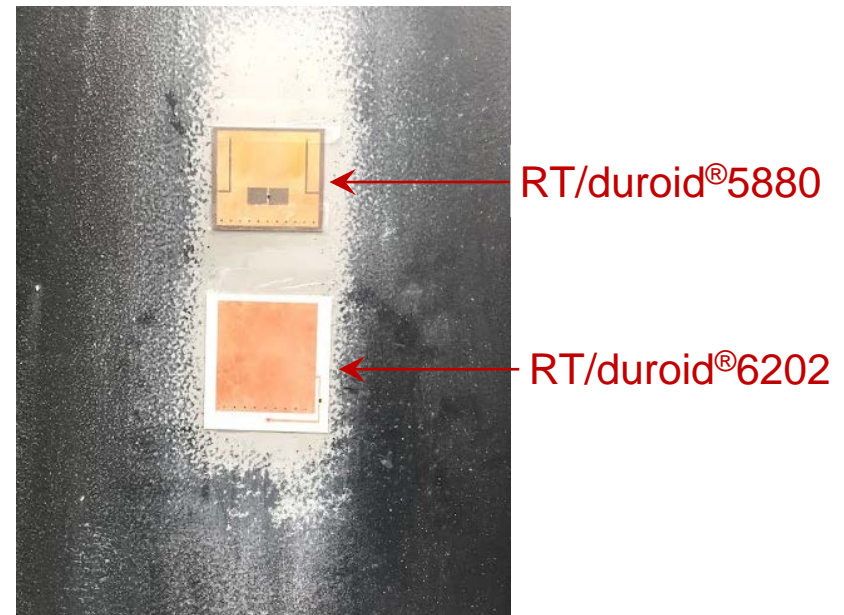
☐ Conclusion

Outdoor Test

Experiment setup



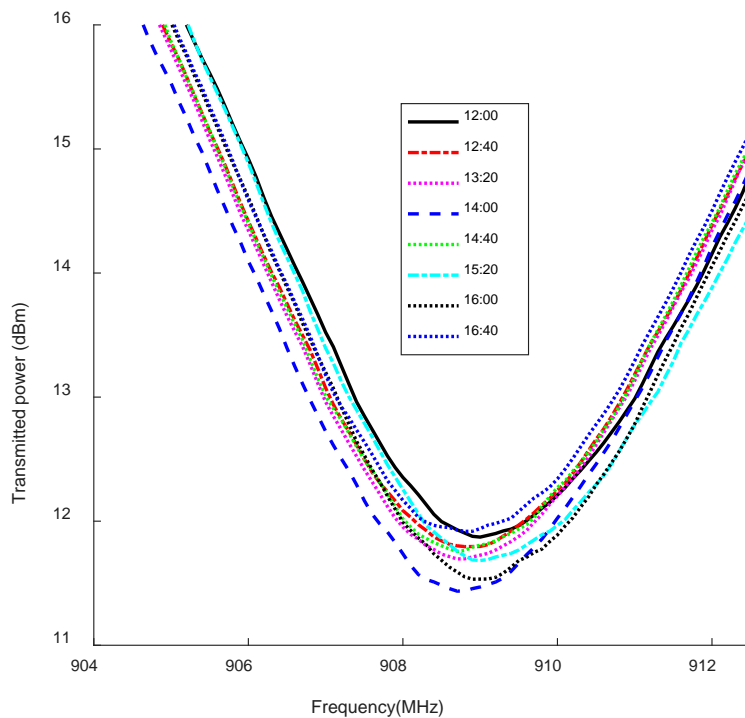
Antenna sensors



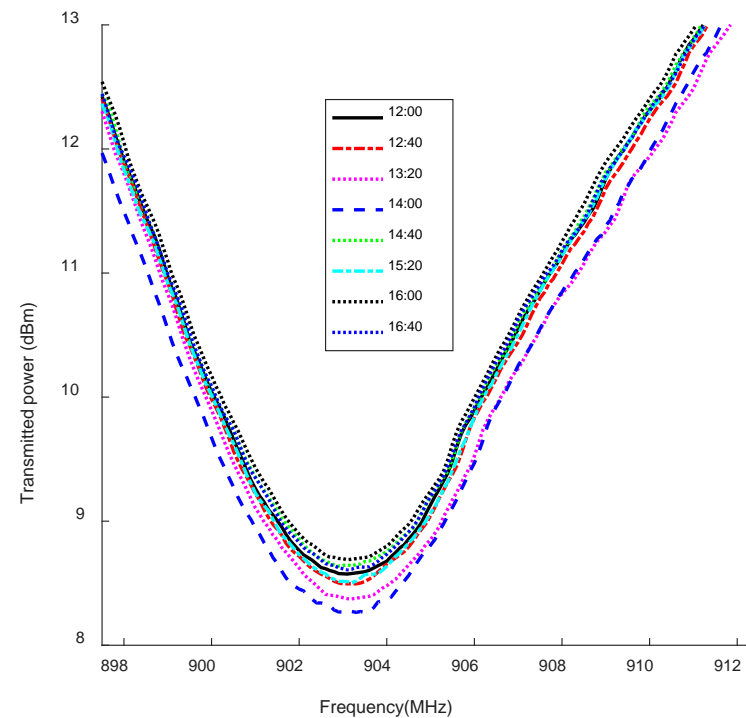
Outdoor Test Results

At each time step, sweep frequency band 897.5 ~ 912.5 MHz

Transmitted power
RT/duroid®5880

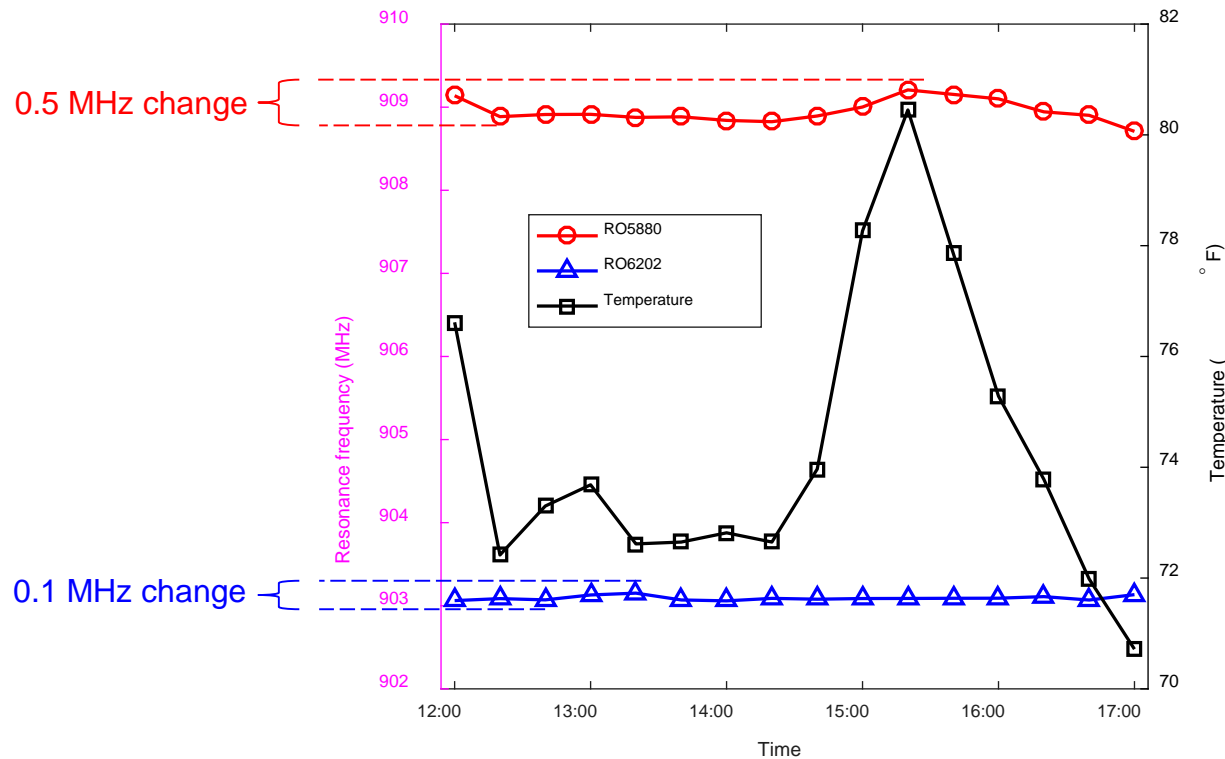


Transmitted power
RT/duroid®6202



Comparison with RT/duroid® 5880

- Comparing with RT/duroid®5880, RT/duroid® 6202 is more stable under outdoor environment disturbance, including temperature variations.

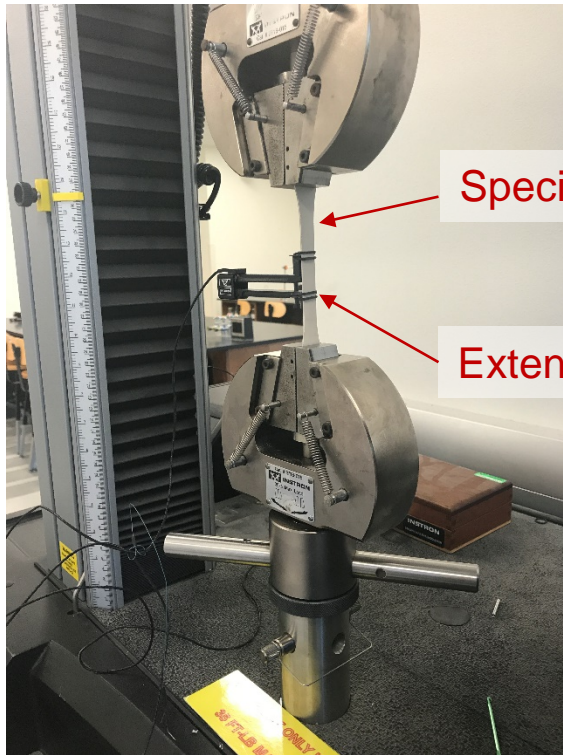


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Mechanical Property Test

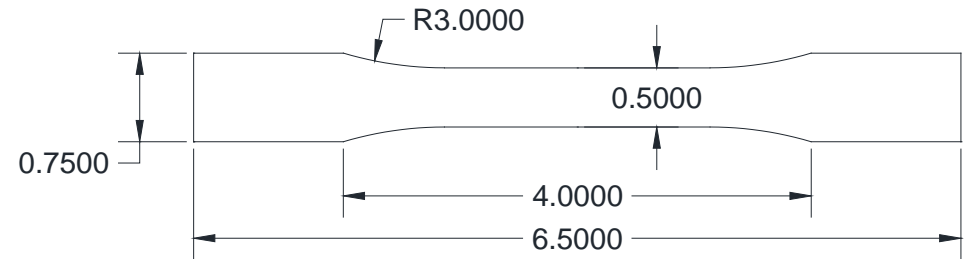
Experiment setup



Specimen

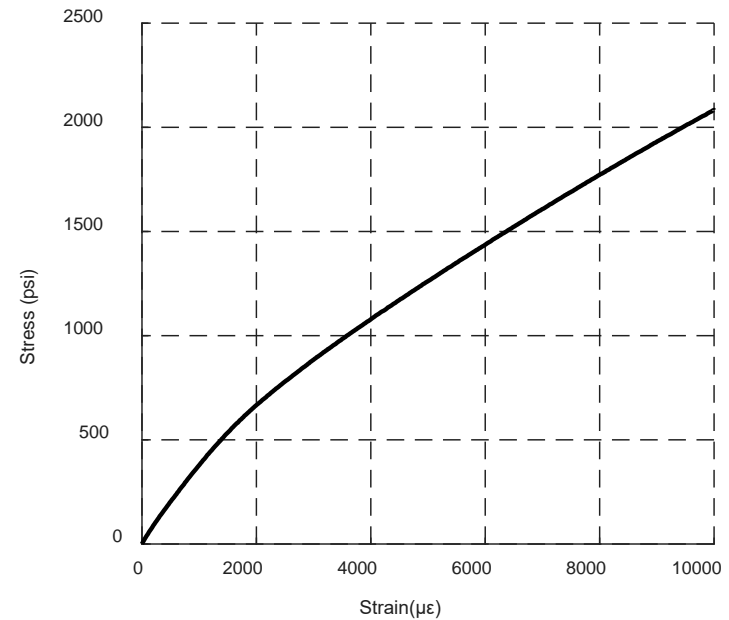
Extensometer

Specimen dimension



Unit: in

Strain-stress relationship



Menegotto-Pinto Model

Menegotto-Pinto model

$$\frac{\sigma(\varepsilon)}{\sigma_0} = b \frac{\varepsilon}{\varepsilon_0} + \frac{(1-b) \frac{\varepsilon}{\varepsilon_0}}{\left[1 + \left(\frac{\varepsilon}{\varepsilon_0}\right)^n\right]^{\frac{1}{n}}}$$

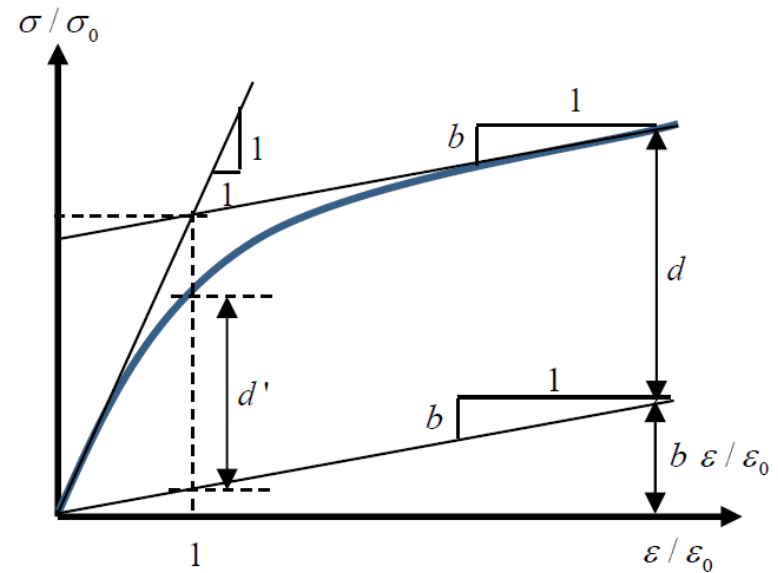
Update parameters: $b, n, \sigma_0, \varepsilon_0$

b : Final tangent stiffness

n : Nonlinear factor

ε_0 : Normalized strain

σ_0 : Normalized stress



Updated Property Along Longitudinal Direction

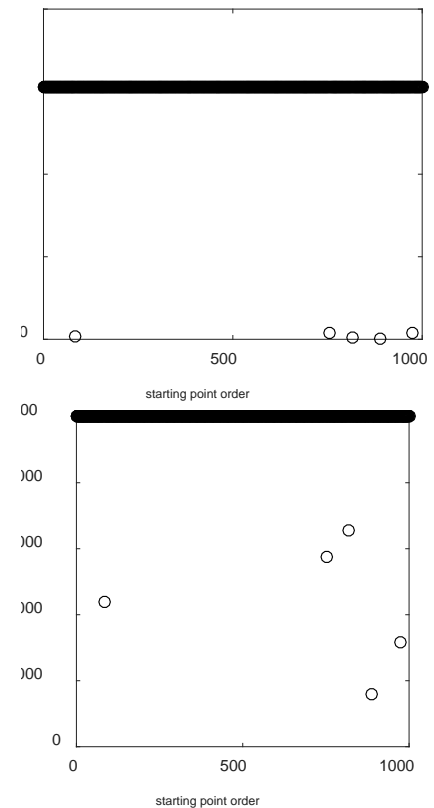
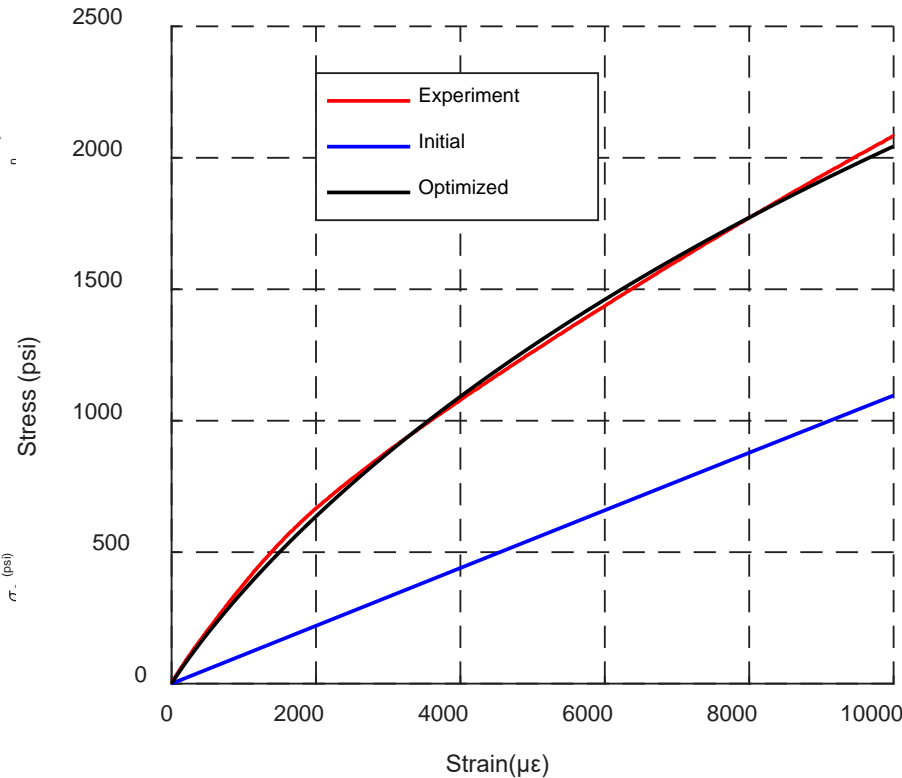
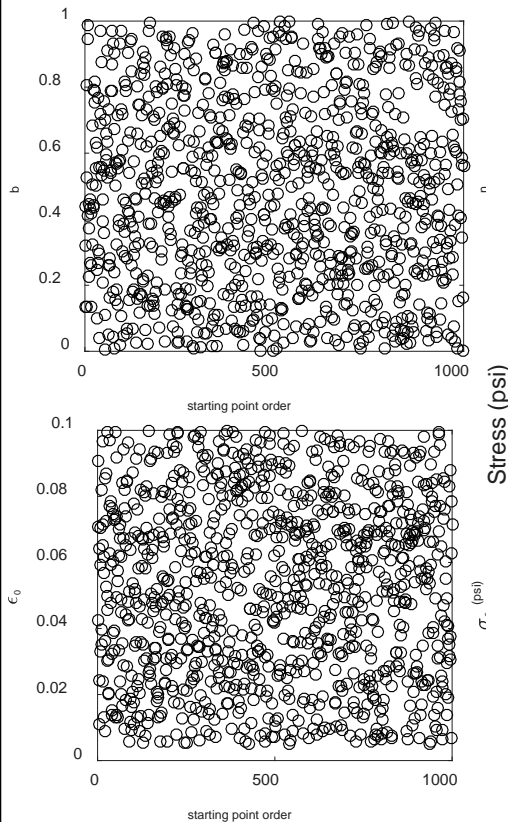
$\mathbf{x}_0 = [b, n, \varepsilon_0, \sigma_0] = [0.5, 2.5, 0.05, 5500]$ (one example)

$\mathbf{x}_L = [b, n, \varepsilon_0, \sigma_0] = [0, 0.0001, 0.005, 1000]$ $\mathbf{x}_U = [b, n, \varepsilon_0, \sigma_0] = [1, 5, 0.1, 10000]$

$\mathbf{x}^* = [b, n, \varepsilon_0, \sigma_0] = [2 \times 10^{-14}, 0.61, 0.02, 10000]$

Starting points (1000) are generated

Optimized parameters



Updated Property Along Transverse Direction

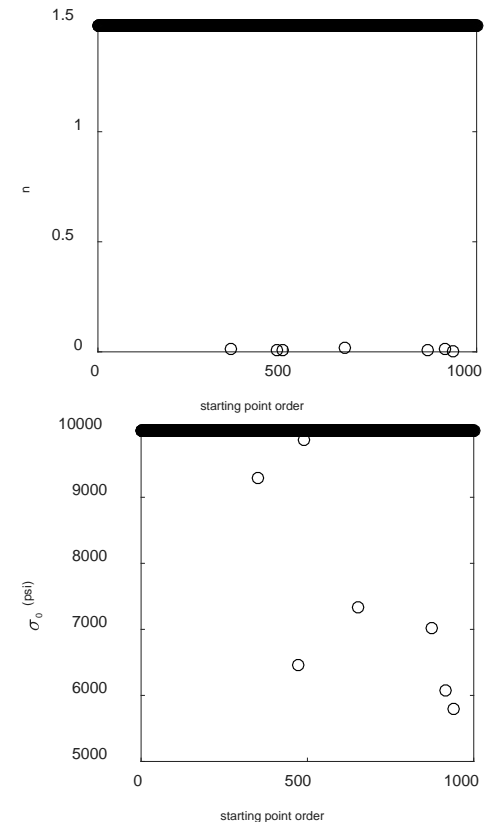
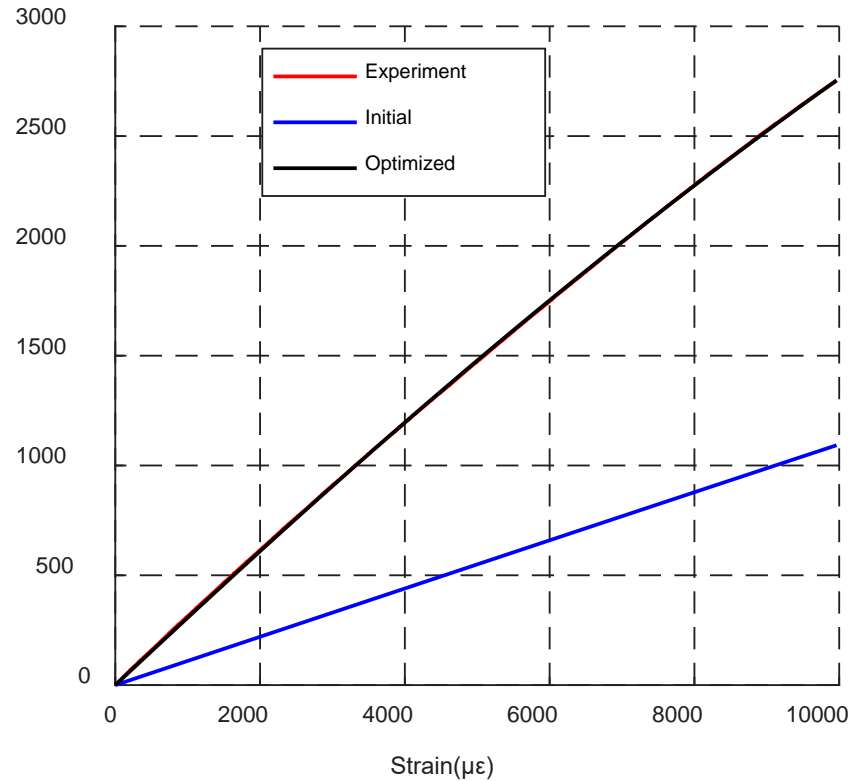
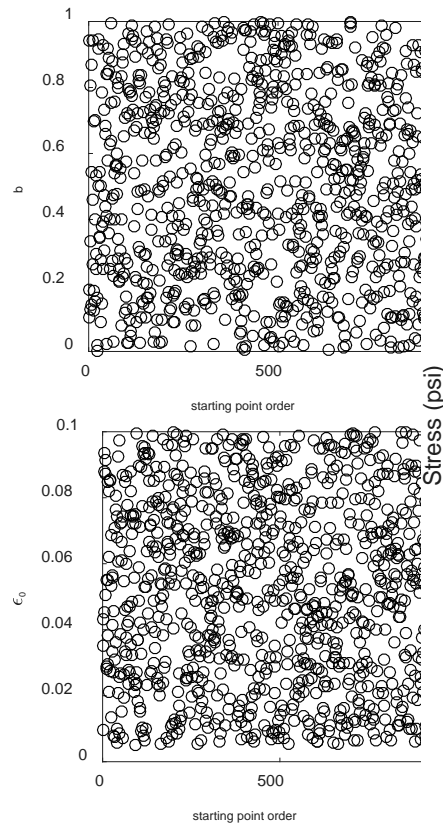
$\mathbf{x}_0 = [b, n, \varepsilon_0, \sigma_0] = [0.5, 2.5, 0.05, 5500]$ (one example)

$\mathbf{x}_L = [b, n, \varepsilon_0, \sigma_0] = [0, 0.0001, 0.005, 1000]$ $\mathbf{x}_U = [b, n, \varepsilon_0, \sigma_0] = [1, 5, 0.1, 10000]$

$\mathbf{x}^* = [b, n, \varepsilon_0, \sigma_0] = [2 \times 10^{-14}, 1.48, 0.03, 10000]$

Starting points (1000) are generated

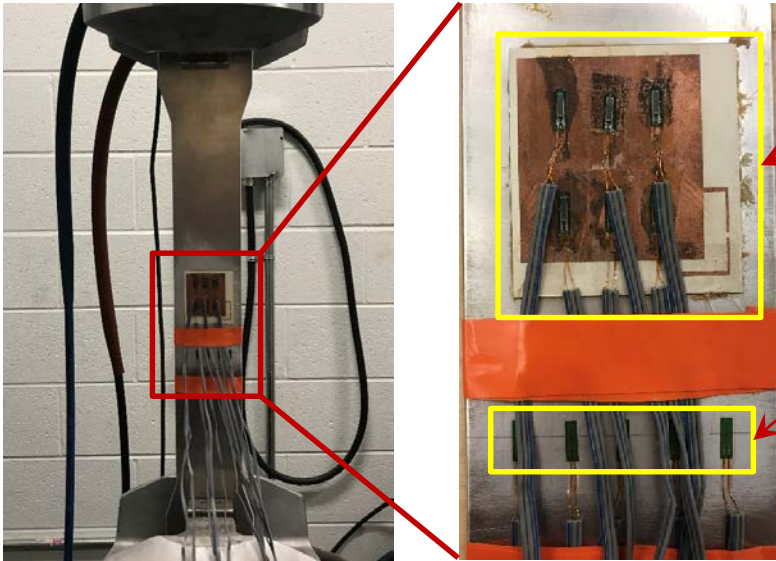
Optimized parameters



Outline

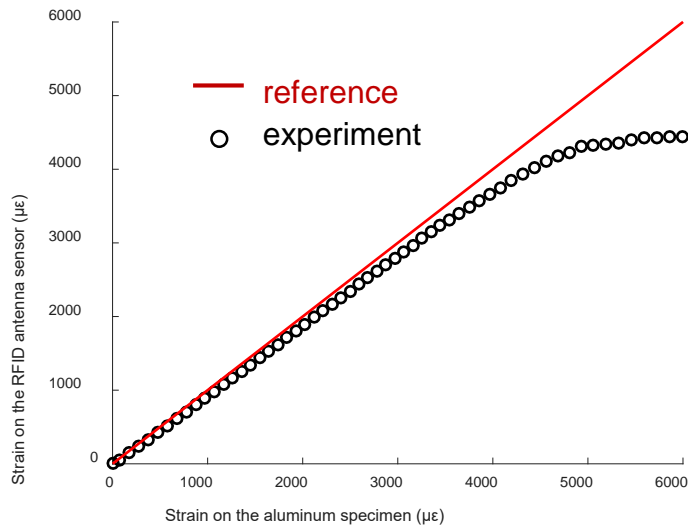
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Strain Transfer Ratio Test

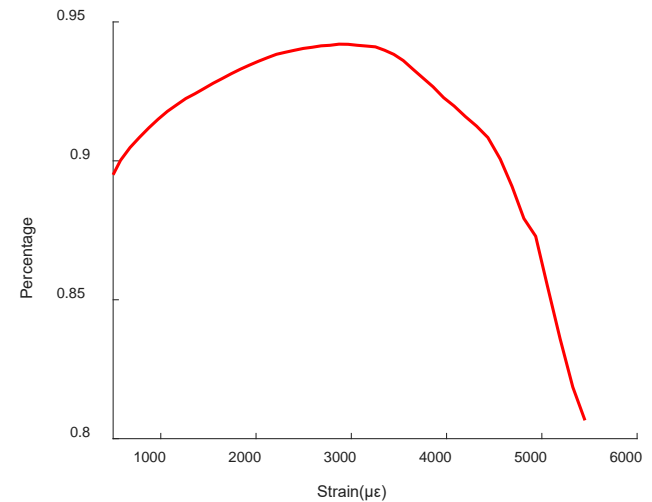


Six strain gages (#1 ~ #6) are installed on top of an RFID patch antenna sensor.

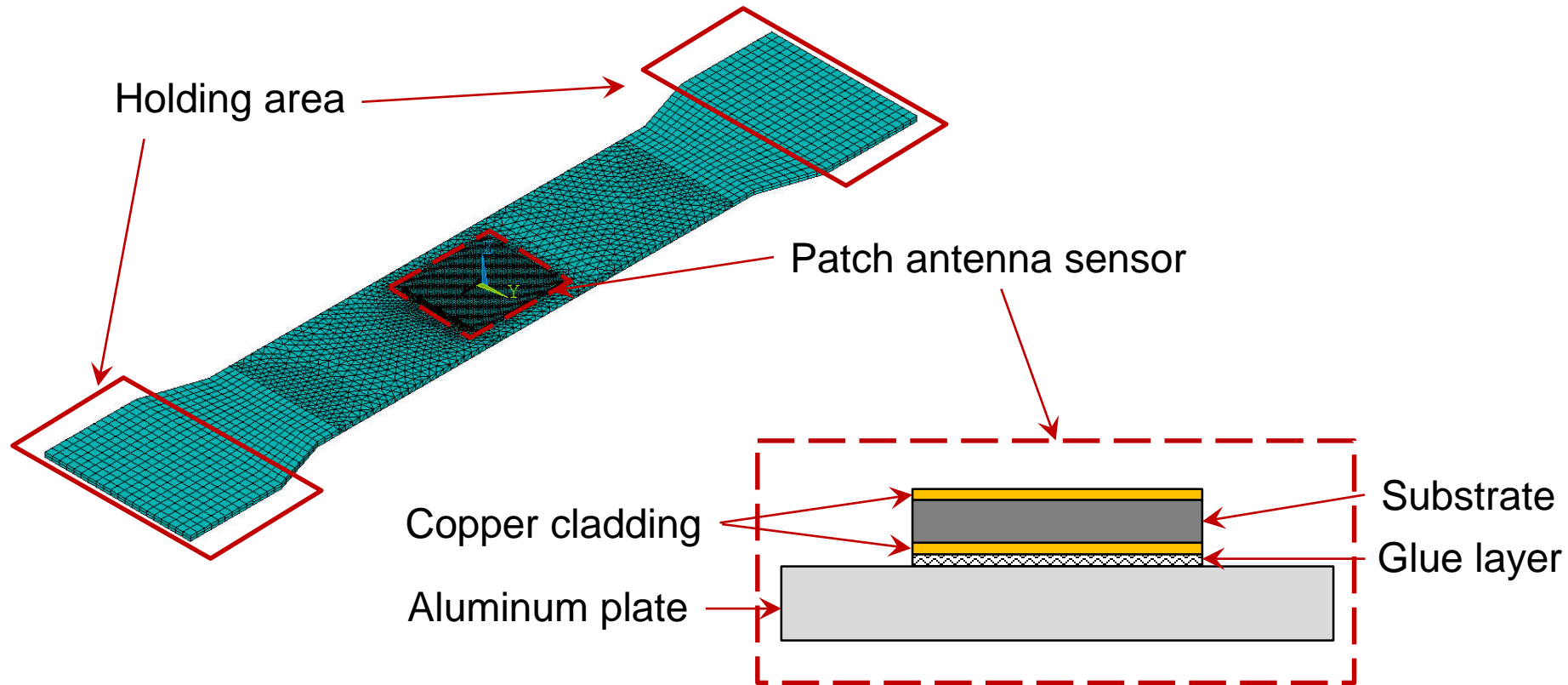
Five traditional strain gages (#7 ~ #11) are installed near the center of the aluminum tensile specimen.



Strain ratio between antenna sensor and aluminum specimen



Strain Transfer Ratio Simulation



- Nonlinear constitutive relationships are used for aluminum, copper, and substrate. (The constitutive relationships are measured by tensile tests.)

Model Updating for Adhesive

- Menegotto-Pinto model with parameters $(b, n, \varepsilon_0, \sigma_0)$ is adopted for nonlinear constitutive model of adhesive.
- Update the parameters $\mathbf{x} = [b, n, \varepsilon_0, \sigma_0]$ by minimizing the difference between experimental strain transfer ratios and simulated strain transfer ratios.

$$\min_{\mathbf{x}} \sum_{i=1}^m [T_{\text{Exp}}(\varepsilon_i) - T_{\text{Sim}}(\varepsilon_i, \mathbf{x})]^2$$
$$\text{s. t. } \mathbf{x}_L \leq \mathbf{x} \leq \mathbf{x}_U$$

where m : the number of strain steps

ε_i : strain level at i -th step

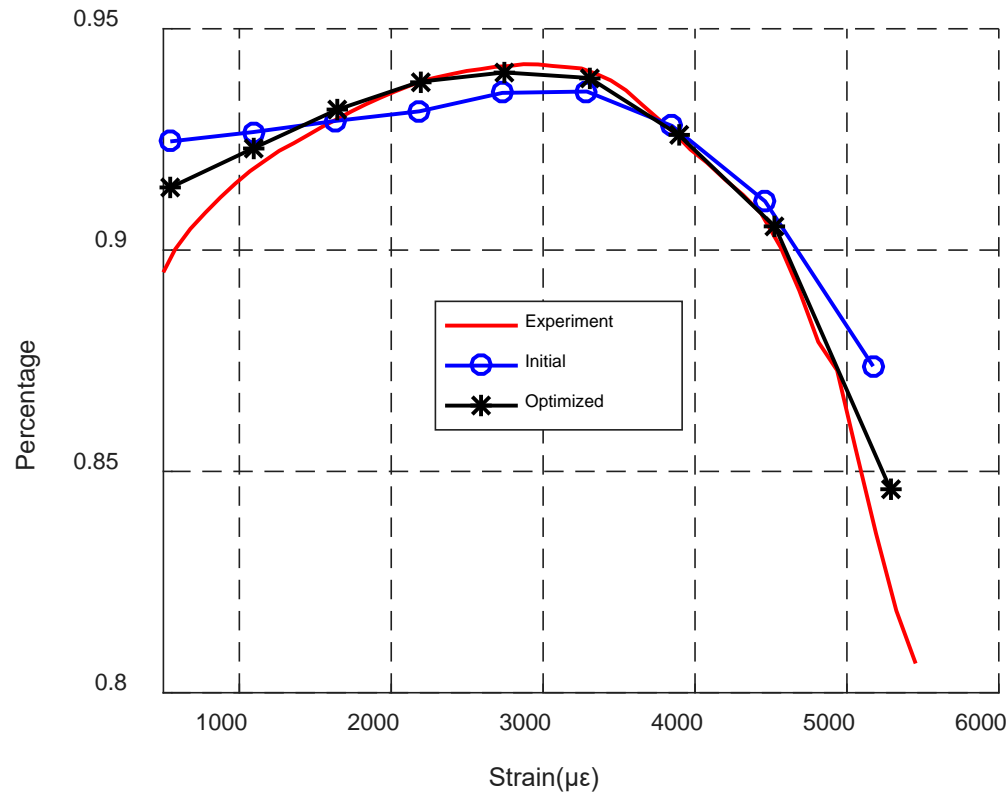
T_{Exp} : strain transfer ratio at ε_i from the experiment

T_{Sim} : strain transfer ratio at ε_i from the simulation

- The optimization problem is solved by Covariance Matrix Adaptation Evolution Strategy (CMA-ES) algorithm.

Hansen, N. (2006), "The CMA evolution strategy: a comparing review", *Towards a new evolutionary computation. Advances on estimation of distribution algorithms*, Springer, pp. 1769–1776.

Model Updating Result



After model updating on adhesive, the simulated strain transfer ratio is closer to the experimental strain transfer ratio.

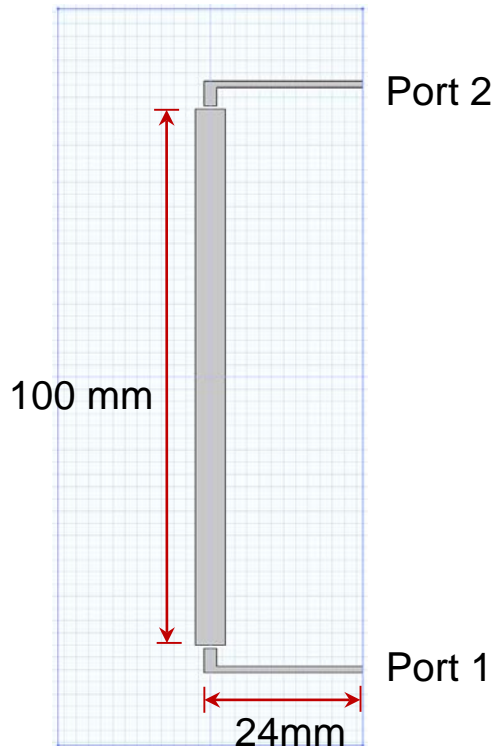
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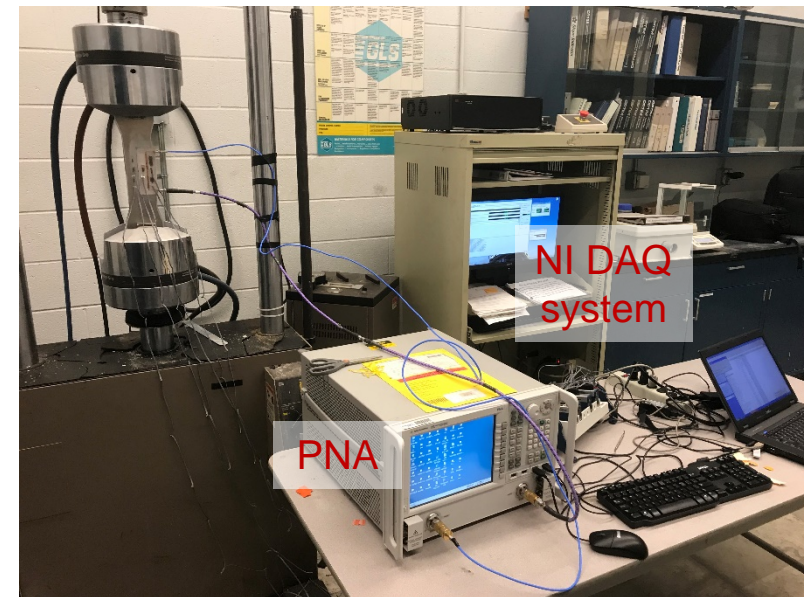
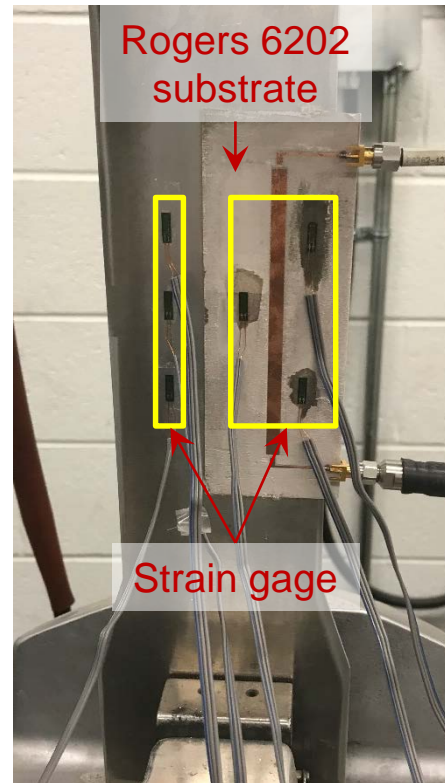
Transmission Line Test

Measure $S_{21}(f) = \frac{V_2^{\text{out}}(f)}{V_1^{\text{in}}(f)}$ to update dielectric constant

Specimen



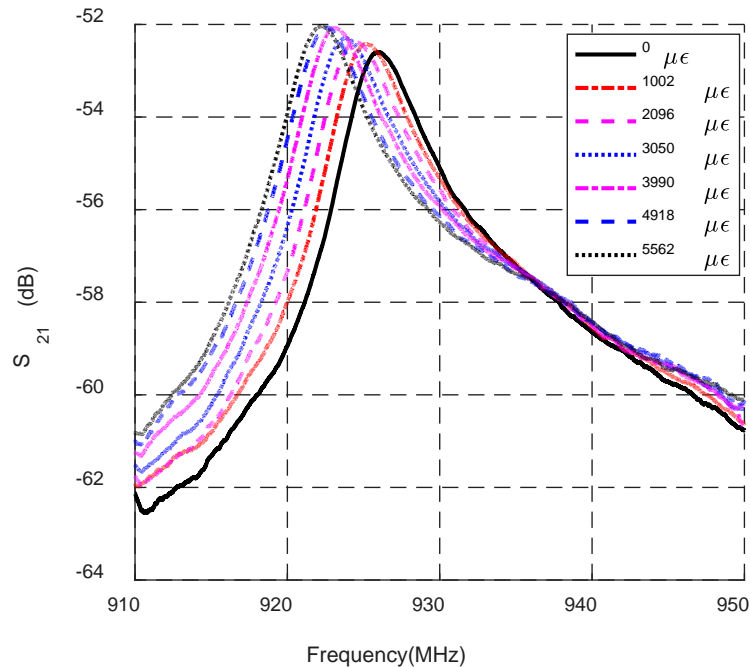
Experiment setup



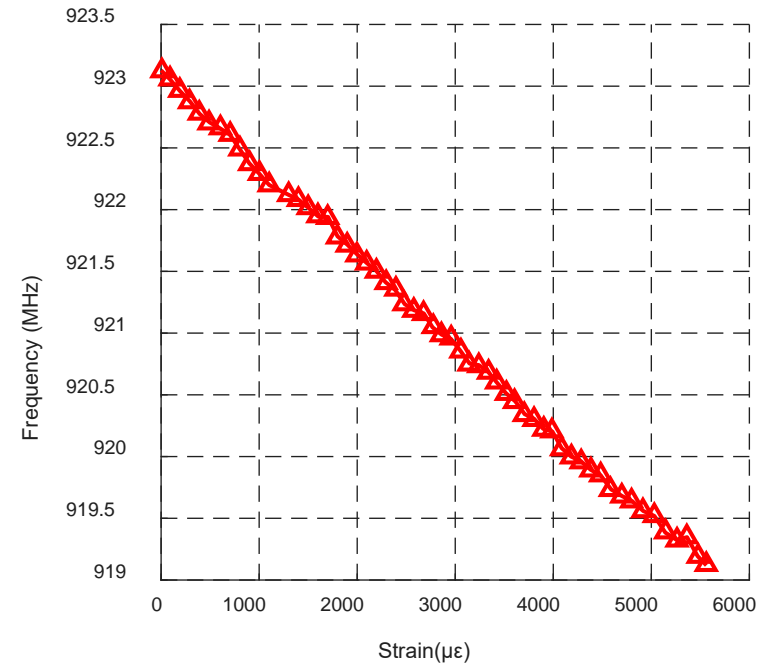
Transmission Line Test Results

- At each strain step, sweep through frequency band 910 ~ 950 MHz
- From S_{21} curve, resonance frequency is extracted

S_{21} curve



Resonance frequency at different strain level



Dielectric Constant Modelling

$$\beta = \beta_0 + \alpha_1 \varepsilon + \alpha_2 \varepsilon(1 - 2\nu)$$

where β_0 : dielectric constant value at zero strain

ε : strain level

ν : Poisson's ratio of the substrate

α_1 and α_2 : updating parameters

Update the parameters $\alpha = [\alpha_1, \alpha_2]$ by minimizing the difference between experimental resonance frequencies and calculated resonance frequencies.

$$\min_{\alpha} \sum_{i=1}^m [f_{\text{Exp}}(\varepsilon_i) - f_{\text{Cal}}(\varepsilon_i, \alpha)]^2$$

$$\text{s. t. } \alpha_L \leq \alpha \leq \alpha_U$$

where m : the number of strain steps

ε_i : strain level at i -th step

f_{Exp} : resonance frequency at ε_i from the experiment

f_{Cal} : resonance frequency at ε_i from the calculation

Updated Parameters For Dielectric Constant

$$\alpha_0 = [\alpha_1, \alpha_2] = [-0.6, -1]$$

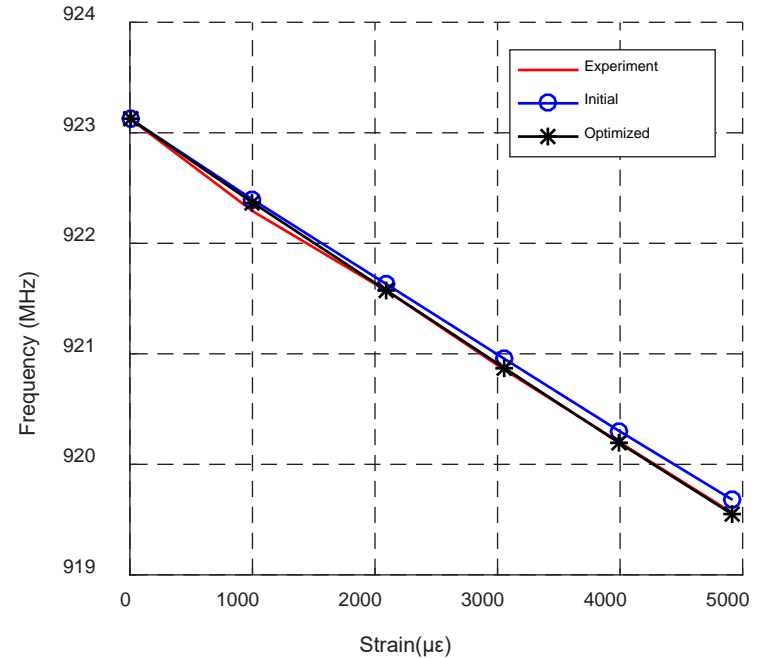
$$\alpha_L = [\alpha_1, \alpha_2] = [-1, -2.5]$$

$$\alpha_U = [\alpha_1, \alpha_2] = [-0.2, -0.5]$$

$$\alpha^* = [\alpha_1, \alpha_2] = [-0.2913, -1.5748]$$

The strain effect on dielectric constant

$$\beta = \beta_0 - 0.2913\varepsilon - 1.5748\varepsilon(1 - 2\nu)$$

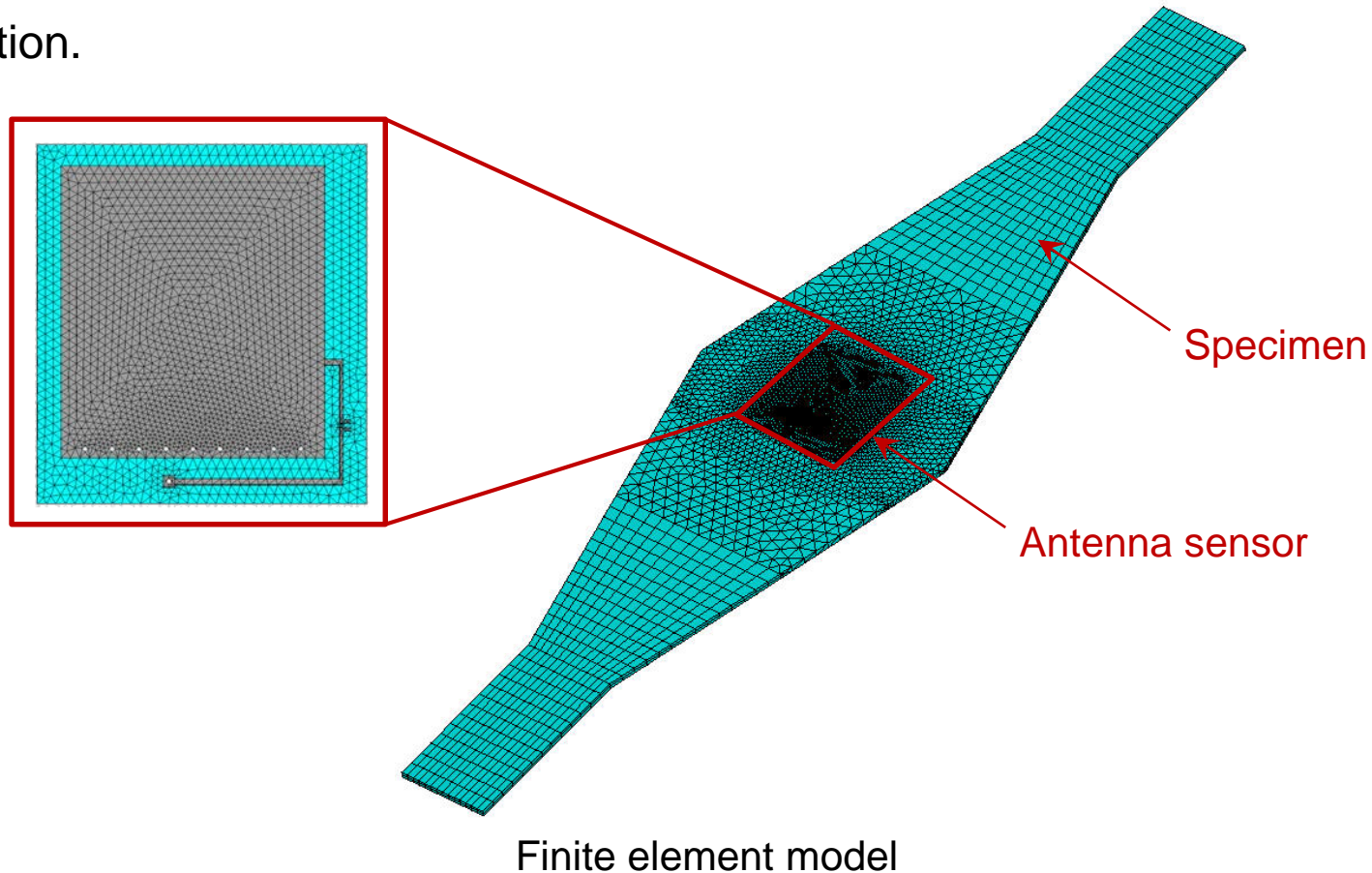


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Multi-physics Simulation

- Mechanical simulations with **linear constitutive properties** and **updated nonlinear constitutive properties** are conducted.
- Dielectric constant change with strain is considered in the electromagnetic simulation.

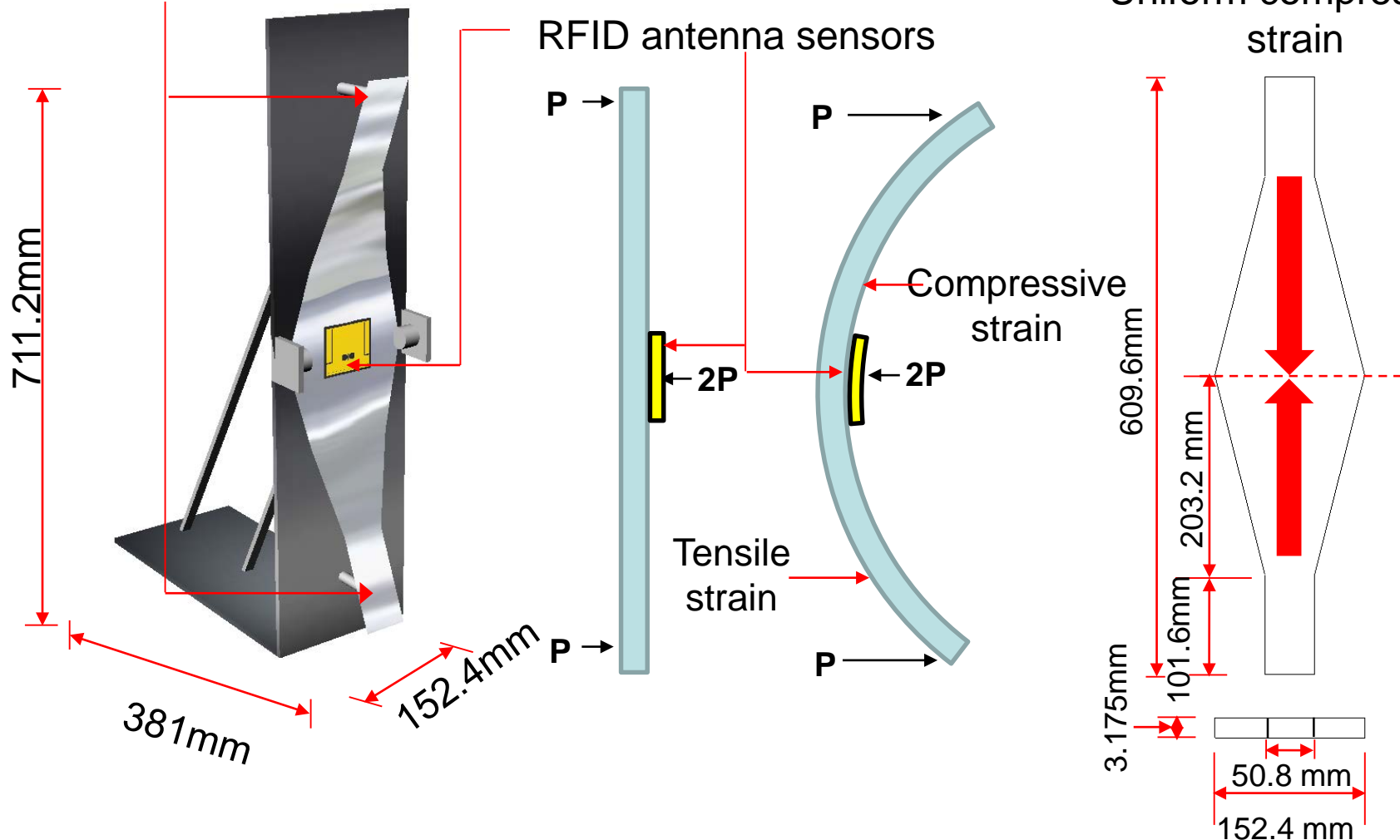


Three-point Bending Setup and Specimen Design

Control screw bolts for bending

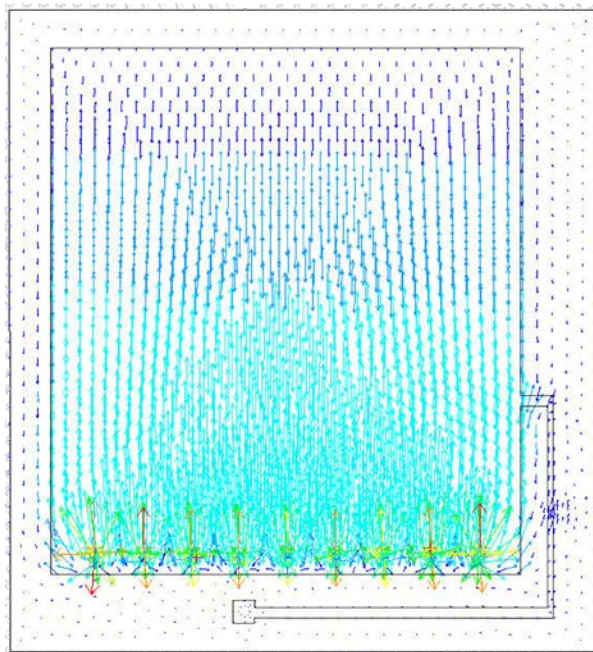
RFID antenna sensors

Uniform compressive strain

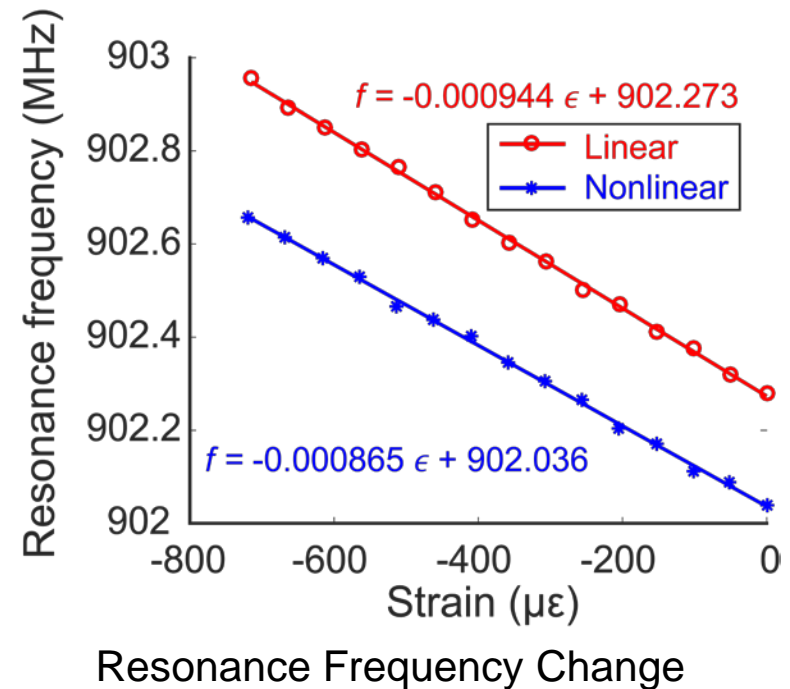


Simulation Results

- The relationship between average strain and resonance frequency is investigated.
- Strain sensitivity is calculated as $-944 \text{ Hz}/\mu\epsilon$ using **linear constitutive properties**, and $-865 \text{ Hz}/\mu\epsilon$ using **nonlinear constitutive properties**.



Surface Current

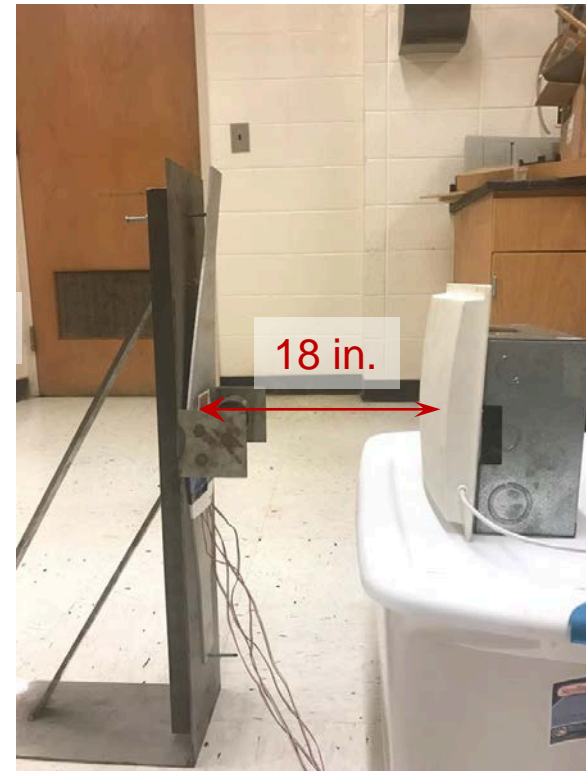
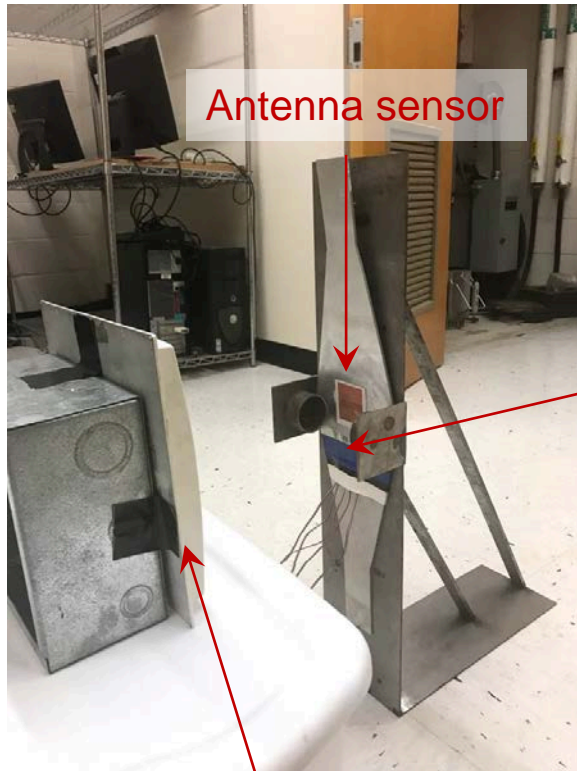


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Compression Test

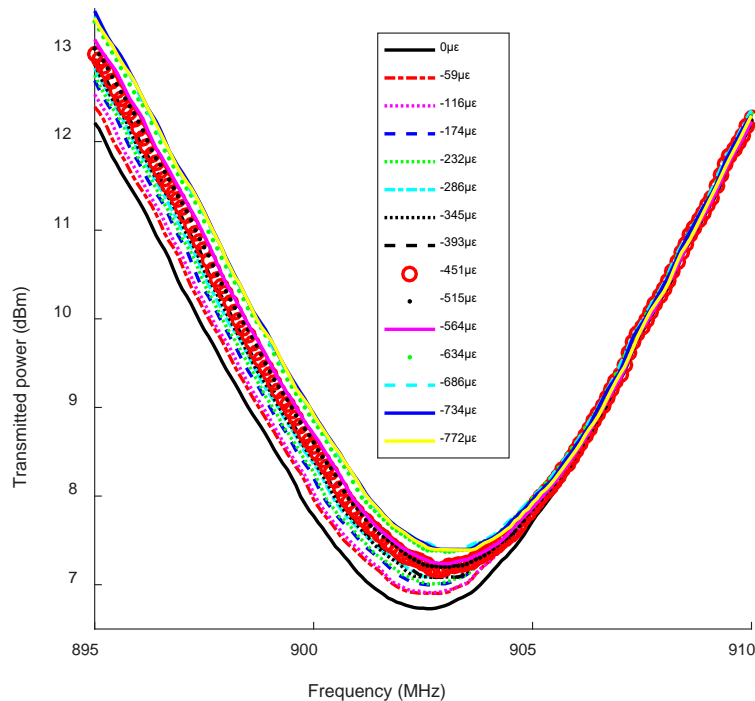
Experiment setup



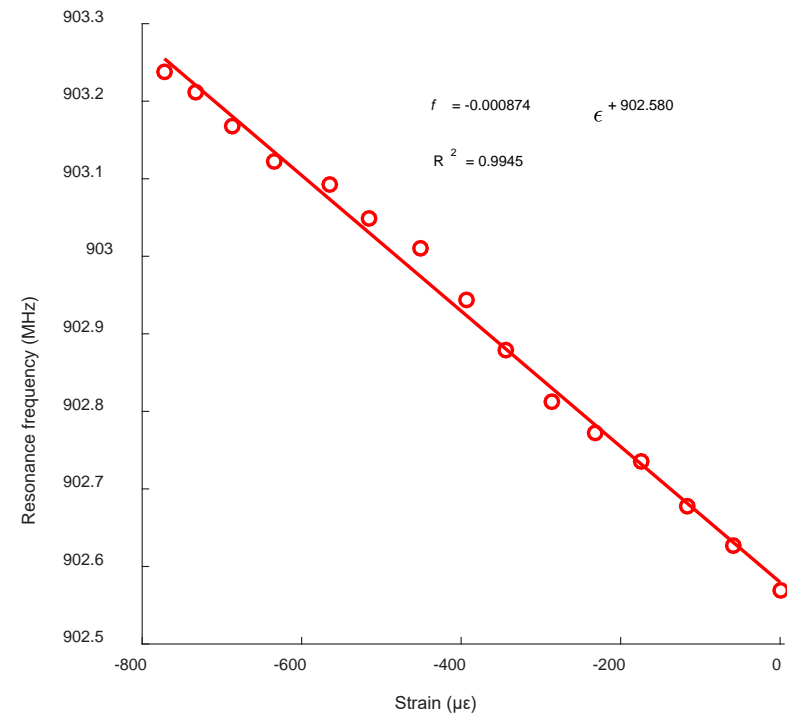
Compression Test Results

- At each strain level, sweep frequency band to get transmitted power curve.
- From transmitted power curve, the resonance frequency is extracted.

Transmitted power



Resonance frequency-strain curve

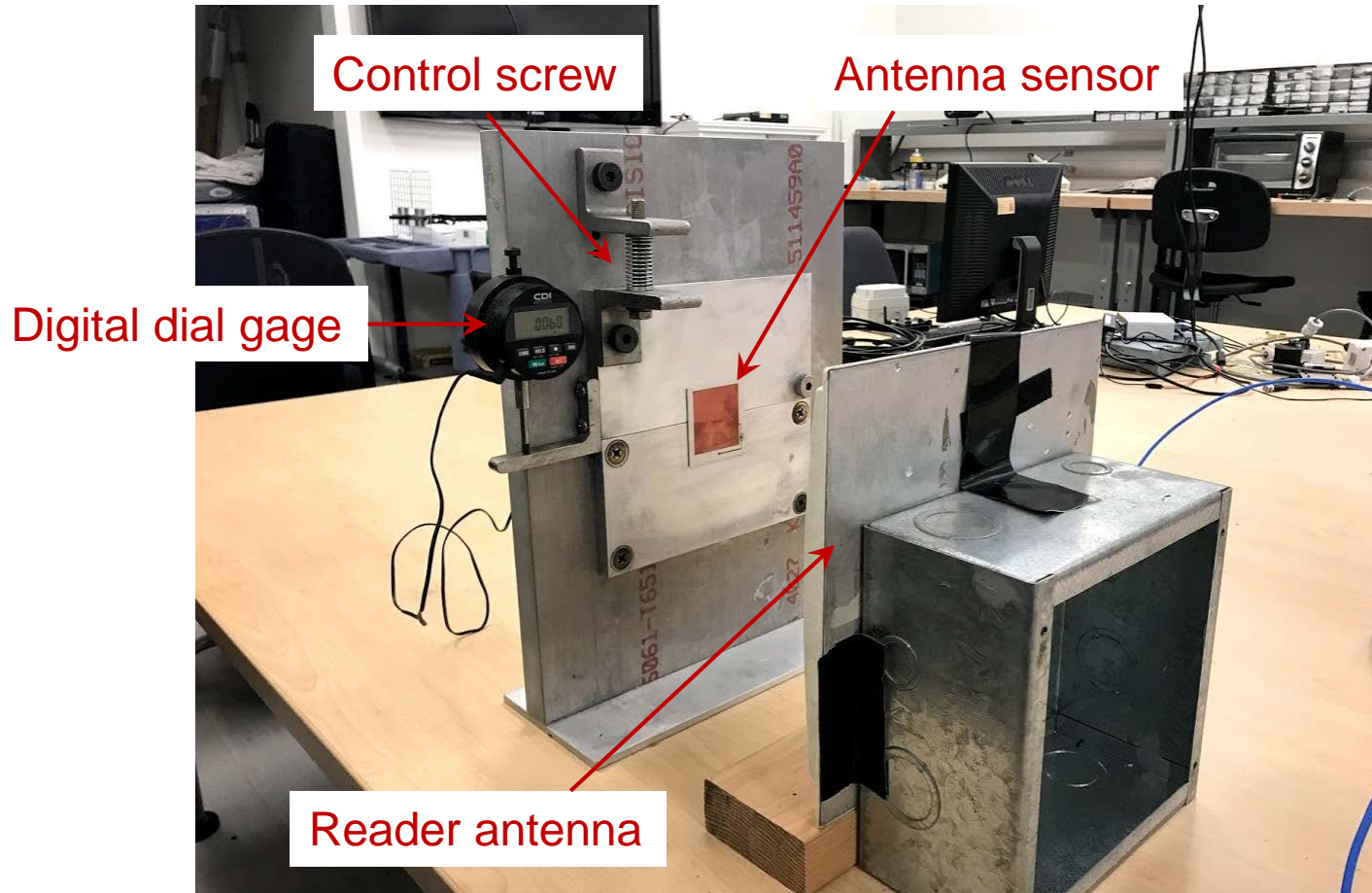


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Crack Test

Experiment setup



Crack Propagation

2 mils



6 mils



10 mils



20 mils



30 mils



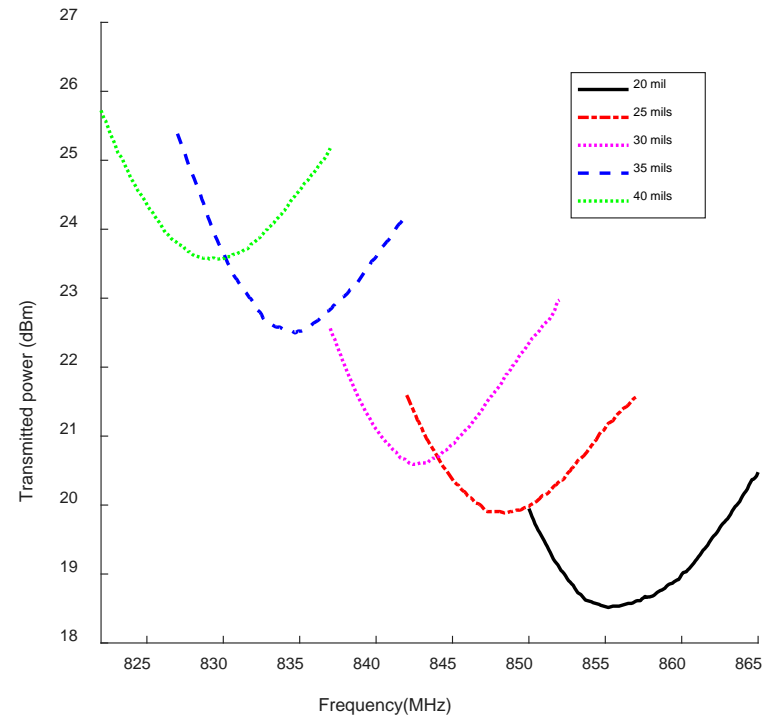
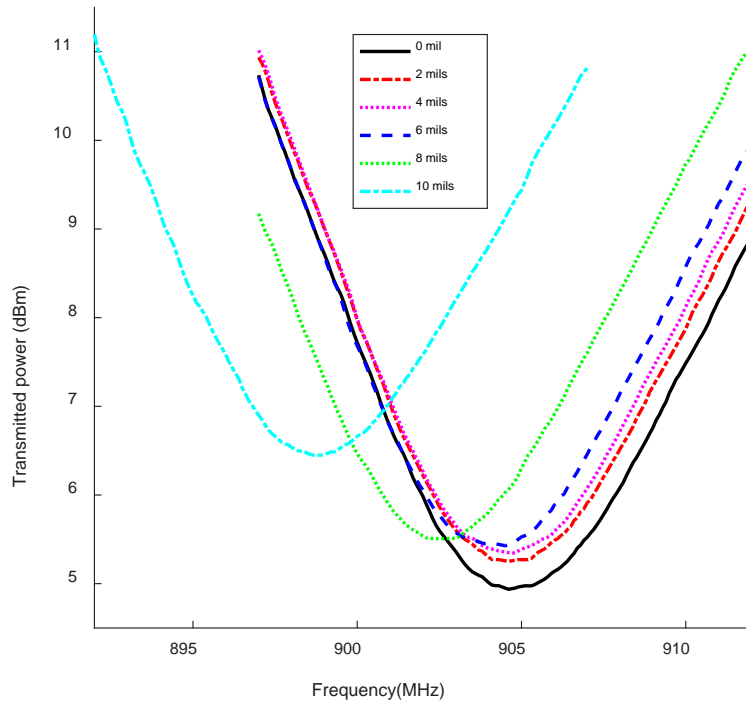
40 mils



Crack Test Results

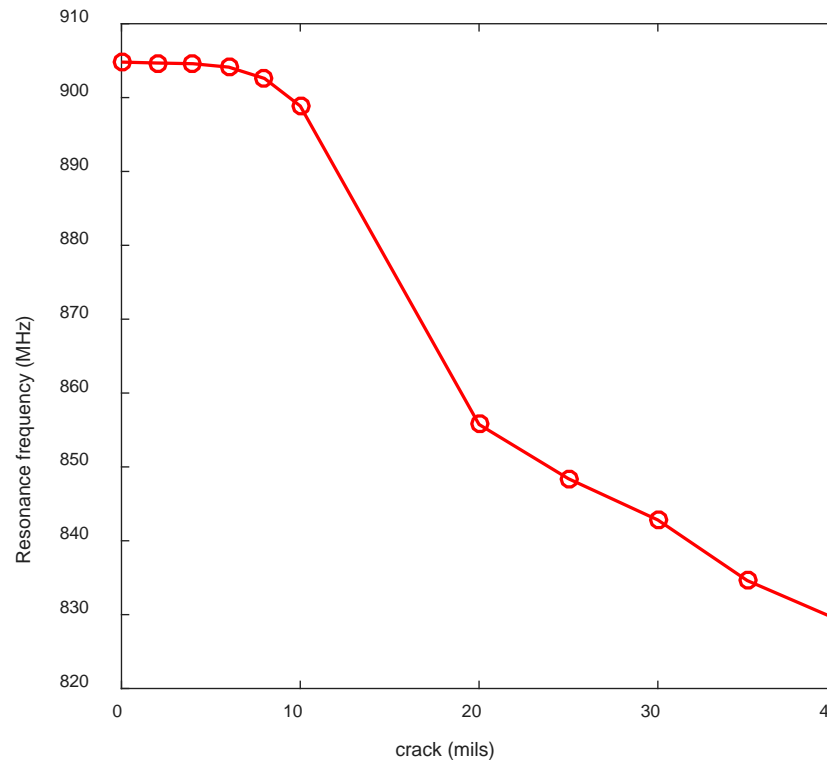
At each crack level, sweep frequency band to get transmitted power curve.

Transmitted power



Crack Rest Results

- From transmitted power curve, resonance frequency is extracted.
- The resonance frequency decreases as crack propagates along sensor's width direction.



Conclusions

1. The sensor with **RT/duroid® 6202** substrate is shown to be more stable under outdoor environment disturbance compared with previous sensor with substrate material **RT/duroid® 5880**.
2. Multi-physics simulation can accurately model behaviors of the antenna sensor. Incorporating **nonlinear constitutive properties** in the model can improve the accuracy of the simulation results on strain sensitivity.
3. The antenna sensor is capable of estimating **small strain changes** on structures. The resonance frequency of the antenna sensor increases as the compression strain is applied.
4. The antenna sensor can monitor **surface crack** growth. As crack propagates, the resonance frequency of the antenna sensor reduces as expected.

Acknowledgements

INSPIRE University Transportation Center
through USDOT/OST-R grant #69A3551747126



Thank You

Questions and Comments?